# Influence of Different Absorption in Desiccated Tissue on Soft-Tissue Surgery with Er:YAG and CO<sub>2</sub> Lasers

Matjaz Lukac<sup>1</sup>, Jernej Kukovic<sup>2</sup>, Nejc Lukac<sup>3</sup>, Franci Bajd<sup>4</sup>

<sup>1</sup>Institut Jozef Stefan, Jamova 39, 1000 Ljubljana, Slovenia <sup>2</sup>University Medical Centre Ljubljana, Department of Dermatovenereology, Zaloska 2, 1000 Ljubljana, Slovenia <sup>3</sup>Fotona d.o.o., Stegne 7, 1000 Ljubljana, Slovenia <sup>4</sup>University of Ljubljana, Faculty of Physics and Mathematics, Jadranska 19, 1000 Ljubljana, Slovenia

# ABSTRACT

In this study, we examined and reviewed the effect of laser wavelength on the cutting rate and peripheral thermal damage during soft-tissue surgery with mid-IR Er:YAG (2,940 nm) and CO<sub>2</sub> (9,000-11,000 nm) lasers.

In agreement with published experimental data, our analysis of the Er:YAG and CO<sub>2</sub> laser-tissue interaction demonstrates that the ablative and thermal diffusion effects on soft human tissues are very similar for both laser types. This is attributed to the fact that both lasers are predominantly strongly absorbed in the soft tissue's intrinsic water content, resulting in the same basic mechanism of interaction with soft tissues which is based on a micro-explosive "boiling" of the confined intrinsic water.

However, as the laser-heated tissue gets partially or completely desiccated during surgery the two laser wavelengths start exhibiting very different properties. While tissue desiccation merely reduces the cutting speed of the Er:YAG laser, the CO<sub>2</sub> laser's higher absorption in the residual dry substance can in addition lead to very high tissue temperatures accompanied by tissue charring. For this reason, CO2 laser surgery is more often accompanied by a higher level of thermal injury to the surrounding tissues, with charring and melting of wound margins, especially at lower volume power densities. This may promote defragmentation tissue and frequently makes histopathological evaluation impossible.

**Key words:** Er:YAG, CO<sub>2</sub>, laser, soft tissue surgery, ablation, coagulation

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## I. INTRODUCTION

Human tissues are multi-component composite systems, with generally very complex interactions with laser light. Within the UVB (280-320 nm), UVA (320-400 nm) and visible light (400-700 nm) spectral regions, skin has three primary absorbers: blood (hemoglobin), melanosomes (melanin), and keratin (see Fig. 1) [1, 2].



Fig. 1: Absorption spectra of human soft tissues. The highest absorption peaks are at the Er:YAG (2,940 nm) and  $CO_2$  (10,640 nm) laser wavelengths. The crosses represent approximate data for dry matter (desiccated tissue) [2-4]; the dotted line is a guide to the eye only.

Despite its abundance in all tissues, water is not a significant absorber of light in the visible region. However, above approximately 1000 nm it becomes a primary absorber, considerably simplifying the interaction mechanism. The ability of mid-infrared lasers to incise and excise soft tissue is thus mainly due to the significant optical absorption of water content  $(60 \sim 80\%)$  in soft human tissues [5].

Ablation temperatures above 100 °C [6-8], as well as the dependence of ablation efficiency on tissue tensile strength [9], and histological evidence of tissue tear [6] all indicate that the ablation of soft tissue with mid-IR lasers is not purely a water evaporation process. Supported also by observations from highspeed photography [10, 11] and time-resolved thermometry [9], a mechanism of micro-explosions is now generally accepted as the main thermomechanical mechanism of ablation of soft tissues with mid-IR lasers [12]. As the tissue water, which is trapped within the microscopic cavities within the soft tissue, absorbs the laser radiation, its temperature increases linearly until the boiling point (T  $\approx 100$  °C) is reached. Further heating converts one part of the water mass into vapor. As the vapor cannot expand freely, pressure in the cavity rises and exerts force on the cavity wall. Micro-explosive removal of tissue starts when the pressure exceeds the ultimate tensile strength of the tissue, which for soft tissues occurs at water vapor temperatures of about 250 °C [7, 13, 14].

Among mid-infrared lasers, the CO<sub>2</sub> (9,000-11,000 nm) and Er:YAG (2,940 nm) lasers are most suitable for performing soft-tissue surgery since their wavelengths are located at the two highest water absorption peaks (Fig. 1). The optical penetration depth ( $\delta_{opl}$ ) of both laser types in soft tissues is very small, below 20 µm (≈3 µm for Er:YAG and ≈ 17 µm for CO<sub>2</sub>) [14].

In this analysis, we compare the ablative and peripheral thermal coagulation effects of the Er:YAG (2,940 nm) and  $CO_2$  (10,640 nm) lasers on soft human tissues such as skin or mucosa. The comparison is made based on numerical calculations using the micro-explosions model of mid-infrared laser ablation of soft tissues [12-15], and on the published in-vitro, ex-vivo and in-vivo studies.

# **II. MATERIALS AND METHODS**

In our study, we applied a numerical model of the physical process of tissue resurfacing as originally developed to study thermo-mechanical ablation with mid-IR lasers. The details of the model are described in [12-15], and will not be repeated here.

In the model, a single wavelength ( $\lambda = 2,940$  nm or  $\lambda = 10,640$  nm) of continuous wave (CW) or pulsed laser radiation with power P (in W) is delivered to the surface area (S) of the treated tissue with a surface power density  $P_d = P/S$  (in W/cm<sup>2</sup>) or pulse fluence F (in J/cm<sup>2</sup>). For a circularly shaped irradiated area, S = $\pi d^2/4$ , where d is the diameter (spot size) of the irradiated area. We modelled the tissue as a watercontaining homogeneous media characterized by a single absorption coefficient of  $k = 1/\delta_{qpt}$  for the delivered Er:YAG or CO<sub>2</sub> laser wavelength  $\lambda$ . Assuming a 70% water content of the modelled soft tissue, the optical penetration depths were taken to be 3 µm for Er:YAG and 17 µm for CO<sub>2</sub>. Since the main focus of our study was on the Er:YAG and CO2 laser wavelengths with their very short penetration depths, the effects of the scattering of laser light within the tissue were not included. Similarly, it was taken that the laser spot size (*d*) is much larger than the optical penetration depth  $(\delta_{opt})$  and, therefore, the diffusion of dissipated heat was treated in one dimension using a finite-difference scheme. Our model accounted for the fact that a substantial amount of the incident beam energy (approximately a half) is expected to be lost at the air-tissue boundary on account of refractive index differences.

The model enabled the calculation of the temporal evolution of the tissue temperature during and following laser irradiation of different laser modalities (CW or pulsed) for different depths z within the tissue, calculated from the extrapolated thermal gradient.

The tissue surface is treated as perfectly insulated. This is accomplished by introducing an additional spatial point just outside the tissue surface with the temperature equal to the value at the neighboring superficial point, thus preventing any heat flow through the surface. When the pressure *p* exceeds the ultimate tensile strength of the tissue, the ablation of tissue begins. The depth to which the tissue gets ablated is denoted by  $d_{abl}$  (in µm).

According to the thermo-mechanical ablation model [12-15], a one-dimensional temperature field was updated at each simulation time step by using a compact threepoint stencil discretization approach that provided a fast, yet sufficiently accurate calculation of the temperature field change upon the delivery of laser pulse irradiation. The light-tissue interaction was modeled by using Beer's law. Stability of the numerical integration scheme was provided by choosing a sufficiently high spatial resolution equal to  $\varDelta z = 0.12 \ \delta_{opt}$  (0.4 µm and 20 µm for Er:YAG and CO<sub>2</sub>, respectively) as well as by the temporal resolution  $\ \ that was determined by the Courant-$ Friedrichs-Lewy number equal to 0.45. The accuracy of the temperature field calculation could be slightly further improved by additionally increasing the spatial resolution, at the expense of a substantially increased computational load. In the study, the following laser parameters were used: pulse duration of  $t_p = 1000/1500 \ \mu s$  with pulsed mode, or  $t_p = 0.3/1$  s with CW mode, pulse repetition rate f = 20/50 Hz, maximal simulation time of 1 s. In the simulations, fluence values were chosen in order to obtain the maximal surface power densities up to 600 W/cm<sup>2</sup>. For each simulation run, the response of the model tissue was characterized by the ablation depth as a instantaneous temperature field (acquired at each 1000  $\Delta t$ ), from which the ablation speed and the depth of heat penetration were calculated. The following tissue properties were assumed in the model: tissue density  $\rho =$ 

1100 kg/m<sup>3</sup>, specific heat of the tissue's solid component  $c_s = 1700 \text{ J/kgK}$ , specific heat of water  $c_w = 4200 \text{ J/kgK}$ , tissue specific heat  $c_m \approx 3500 \text{ J/kgK}$  and tissue thermal conductivity  $\lambda_{tb} = 0.42 \text{ W/mK}$ .

#### **III. RESULTS**

#### a) Ablation rate

The calculated ablation (cutting) speed  $AS = d_{abl}/time$  (in  $\mu m/s$ ) for CO<sub>2</sub> and Er:YAG lasers operating in continuous wave (CW) or pulsed (pulse duration  $t_p = 1500 \ \mu s$ , pulse repetition rate  $f = 20 \ or 50 \ Hz$ ) mode are shown in Fig. 2.



Fig. 2: Calculated ablation speed  $(\mathcal{AS})$  versus surface power density for CW (squares) and pulsed (circles) operation of Er:YAG and CO<sub>2</sub> laser. Note the similarity of ablation speeds for the two laser sources and for different laser irradiation modes.

As can be seen from Fig. 2, the more than 5-fold difference in the optical penetration depths between the two laser sources does not have a significant influence on the ablation rate  $AR = AS/P_d$  (in  $\mu m/(J/cm^2)$  in soft tissues. Within the micro-explosions boiling model, the ablative effect on soft tissue is the same for Er:YAG and CO<sub>2</sub> laser wavelengths. Similarly, the soft-tissue average cutting speed does not depend on whether the laser energy is delivered in a continuous (CW) or pulsed manner. Therefore, the above figure can be considered to also represent the dependence of the ablation depth  $d_{abl}$  (in  $\mu m$ ) on the laser pulse fluence F (in J/cm<sup>2</sup>).

Note that the speed of mass removal, MS (in g/s) is proportional to the laser power P as:

$$MS = P \left( AR \rho S \right) \quad . \tag{1}$$

The similarity of the slopes of the ablation rates  $AR = AS/P_d = d_{abl}/F$ , (in  $\mu$ m/(J/cm<sup>2</sup>)) of the two laser types was also observed experimentally [16]. Figure 3 depicts the measured dependence of the ablation depth vs. fluence for the ablation of guinea pig skin using a TEA

CO<sub>2</sub> laser and a normal-spiking-mode Er:YAG laser.



Fig. 3: Measured ablation depth vs. fluence for the ablation of guinea pig skin using a CO<sub>2</sub> ( $t_p = 2\mu s$ ) and an Er:YAG laser ( $t_p = 250 \ \mu s$ ) [16]. Note the similar ablation rates for these two different sources of infrared laser radiation.

The observed similarity of the ablation rates of Er:YAG and  $CO_2$  lasers confirms that confined "boiling" with micro-explosions is the main ablation mechanism for both laser types, despite the difference between their absorption coefficients.

Our model predicts the CO<sub>2</sub> and Er:YAG laser ablation rates in soft tissues of approximately  $AR \approx 5$  $\mu$ m.cm<sup>2</sup>J<sup>-1</sup>. This is in good agreement with the reported measured ablation rates for CO<sub>2</sub> and Er:YAG in soft tissues ranging between 2 and 4  $\mu$ m.cm<sup>2</sup>.J<sup>-1</sup> [15-20]. Slightly lower measured ablation rates than calculated can be attributed to the effect of tissue desiccation during laser irradiation, and partially also to additional heat losses not included in our model. Such losses include, for example, heat diffusion in the transverse direction and heat flow into the surrounding.

Finally, the independence of the ablation rate on the optical penetration depth can also be concluded based on analytical relations. It is well known that in the absence of heat diffusion, the ablation threshold fluence ( $F_{tb}$ ) can be calculated from [21]:

$$F_{tb} = h_a \cdot \delta_{opt} , \qquad (2)$$

where  $b_a$  marks the specific heat of ablation (in J/mm<sup>3</sup>). The ablation threshold fluence represents the fluence required to ablate a tissue layer with a thickness  $\delta_{opt}$ . When a tissue is irradiated with a certain laser surface power density  $P_d$ , a tissue layer with thickness  $\delta_{opt}$  gets heated up to the ablation threshold in the ablation time  $t_{abb}$  defined by  $F_{tb} = P_d t_{abl}$  [21], and therefore:

$$t_{abl} = h_a \cdot \delta_{opt} / P_d \ . \tag{3}$$

Finally, this gives the ablation speed AS that is independent of the laser wavelength:

$$AS = \delta_{opt} / t_{abl} = P_d / b_a . \tag{4}$$

By taking  $b_a \approx 3.4 \text{ J/mm}^3$  [15, 22], we obtain the ablation rate of  $AR \approx 3 \text{ µm.cm}^2 \text{ J}^{-1}$ , in good agreement with our numerical calculations and published measurements.

In what follows, we shall assume the ablation rate for both lasers to be  $AR = 3 \ (\mu m/s)/(W/cm^2)$ , which represents an approximate average of the reported ablation rates for both laser types.

### b) Thermal depth

The Er:YAG and CO<sub>2</sub> lasers are generally considered to be ablative lasers due to their very high absorption in water, and the resulting very short optical penetration depth ( $\delta_{opt}$ ) into human tissues. However, it is not only the optical penetration depth but also the depth of thermal diffusion ( $\delta_{diff}$ ) that takes place during a laser irradiation of duration  $t_{ir}$  that determines the thermal penetration depth  $(d_{tb})$  of the laser radiation:  $d_{tb}$  $= \delta_{apt} + \delta_{diff}$  [21]. In this study, we calculated  $d_{tb}$  as the depth within the tissue at which the temperature increase  $\Delta T$  caused by laser irradiation drops to 50% of the temperature increase at the surface of the tissue. Our model calculations show that the thermal diffusion depth ( $\delta_{diff}$ ) can be roughly estimated from the characteristic diffusion depth  $\delta_{diff} = 0.5 (2D t_{ir})^{1/2}$  (the pre-factor of 0.5 accounting for the half-space geometry of the model), in which the diffusion constant D = $\lambda_{tb}/\rho_{cm}$  for the skin is equal to 1.1 x 10<sup>-7</sup> m<sup>2</sup>/s [12].

Our analysis shows that there are three, basically simultaneous steps in tissue heating upon laser irradiation [21]. The tissue is first heated directly within the optical absorption depth (*direct heating*) (Fig. 4 a). Direct heating is followed by thermal diffusion that indirectly heats the deeper lying tissues (*indirect heating*) (Fig. 4 b). For short irradiations, the time span for thermal diffusion is short, and the heat energy does not reach very deep into the tissue. For longer irradiations, the heat has sufficient time to spread deeper into the tissue. In the third step, the hottest part of the tissue close to the surface is ablated, in effect reducing the depth of the thermally affected skin layer (Fig. 4 c).

Therefore, the longer the duration of laser irradiation  $(t_{ij})$ , the longer the thermal diffusion depth  $(\delta_{dijj})$ , and consequently also the longer the overall thermal penetration depth  $(d_{tl})$ . This can be seen in Fig. 5, which shows the dependence of the thermal penetration depth on the laser irradiation time in the absence of ablation.



Fig. 4: Three steps in tissue heating upon laser irradiation: a) tissue is first heated directly within the optical absorption depth (*direct heating*); b) direct heating is followed by thermal diffusion that indirectly heats the deeper lying tissues (*indirect heating*); and c) ablation of the hottest part of the tissue close to the surface.



Fig. 5: Dependence of thermal depth on irradiation time in the absence of ablation. The dotted horizontal lines mark the maximal thermal depths achievable with different power densities.

On the other hand, the higher the ablation speed, the shorter the overall thermal depth, since at higher ablation rates most of the thermally affected layer is being removed by means of micro-explosions. This can be seen in Fig. 6, which shows the dependence of the thermal depth on the power density for  $t_{ir} = 0.3$  s.



Fig. 6: Thermal depth as a function of surface power density for irradiation time of  $t_{ir} = 0.3$  s, comparatively for CO<sub>2</sub> and Er:YAG.

For any laser power density, the thermal depth will increase with time following the onset of laser irradiation until the ablation threshold is reached, after which the confined boiling with micro-explosions will prevent the thermal depth from increasing any further (See Fig. 7). This maximal thermal depth depends on the surface power density, being smaller for higher surface power densities (see Fig. 8).



Fig. 7: Temporal evolution of the thermal depth for  $P_d = 300 \text{ W/cm}^2$  (above) and  $P_d = 600 \text{ W/cm}^2$  (below) for CW Er:YAG (red) and CO<sub>2</sub> (blue) mode, and for pulsed ( $t_p = 1.5 \text{ ms}$ , 20 Hz) Er:YAG (violet) and CO<sub>2</sub> (cyan) mode.

Note that when the laser energy is delivered in a repetitive pulsed mode, the instantaneous laser power densities during a pulse are much higher than the power density averaged over the pulses. This results in a "pulsed" ablation and an oscillation of the thermal depth around the maximal thermal depth of the corresponding CW mode with the same average power density  $P_{d}$ . (see Fig. 7).



Fig. 8: Maximal thermal depth as a function of surface power density. The higher ablation speed at higher power densities reduces the overall depth of the thermally affected tissue layer.

As can be seen from the above figures, the thermal depths resulting from the combined effect of thermal diffusion and ablation are approximately the same for Er:YAG and CO<sub>2</sub> lasers, regardless of whether the laser radiation is delivered in a CW or pulsed mode. Note that the calculated thermal depths coincide well with the measured depths of thermal damage of  $\approx 50$  - 100 µm, as observed during cutaneous surgery with Er:YAG and CO<sub>2</sub> lasers [20, 22].

#### c) Tissue desiccation

The water content of soft tissues is very high, and varies between 65 and 80% [5]. However, it is well known that as a result of laser heating, the tissue can get progressively desiccated, leading to a significant reduction in tissue water content [23, 24]. Our measurements of the surface temperature on agar following irradiation with a single Er:YAG laser pulse show that the temperature does not grow linearly with the laser fluence up to the ablation threshold, but exhibits a slight bend at an intermediate temperature (see Fig. 9a). Agar with 70% water content was used, assuming its optical and thermo-mechanical properties be close to those of soft tissues. Similar to measurements with CO2 and Er:YAG lasers have been made also on human skin [7, 25]. In agreement with our measurements in agar, they showed a bend occurring at about 100 °C (Fig. 9 b). This behavior was attributed to the accelerated process of evaporation of the heated soft tissue's free water, effectively desiccating the tissue already during a single laser pulse.



Fig. 9: Measured dependence of the surface temperature on the laser fluence for a) Er:YAG laser on agar; and b) Er:YAG and  $CO_2$  laser on human skin [7]. The intermediate bend in the temperature curve is caused by the evaporation of free water within the tissue.

Therefore, in the initial heating phase the free water starts to evaporate, followed in the next stage by the micro-explosive confined boiling of the bound water. Water evaporation was observed also during ablation studies with a  $CO_2$  laser on guinea pig skin by measuring the tissue mass before, during and after laser irradiation [18]. The measured mass loss rate due to incidental water evaporation was negligible prior to laser irradiation, became appreciable during laser heating and ablation, and continued also after the laser radiation was stopped (see Fig. 10).



Fig. 10: Tissue mass versus time prior, during and post  $CO_2$  laser irradiation of guinea pig skin [18]. Note that the preablation evaporation rate is negligible, while the postablation evaporation rate is considerable due to the tissue temperature remaining elevated, and the superficial dry stratum corneum having been ablated.

The phenomenon of tissue desiccation has an especially pronounced effect on the ablation of hard tissues with low intrinsic water content [26]. For example, Fig. 11 shows a progressive reduction in the measured ablation depth with the increasing number (N) of successively delivered Er:YAG laser pulses on enamel (3% water content) and cementum (22% water content) [27].



Fig. 11: Measured ablation depths in enamel and cementum as a function of delivered laser pulses N, for the same Er:YAG laser pulse fluence of F = 35 J/cm<sup>2</sup> [27].

As a result of tissue desiccation, considerable reduction and even stalling of the ablation process

occurs during the delivery of consecutive Er:YAG laser pulses on cementum and enamel. The effect is most pronounced on enamel, the human tissue with the lowest water content (3%). The ablation on enamel starts with a relatively high intrinsic ablation rate and as the enamel gets progressively desiccated, the ablation stalls at the ablation saturation depth,  $d_{sat}$ . However, a considerable reduction in the ablation rate is observed also on cementum (22% water content).

It is important to note that in order to improve the measurement sensitivity, the ablation rates are typically measured from the depth, volume or mass of cavities made by a large number of consecutively delivered pulses, or by a prolonged delivery of CW laser irradiation [26, 27]. As a result, the measured ablation rates are typically lower than what would be the intrinsic ablation rates in the absence of tissue desiccation [27-29].

Ignoring the effects of thermal diffusion, the time available for tissue desiccation  $(t_{des})$  is equal to the ablation time  $t_{abl}$ , i.e. the time required for the laser to heat up the tissue layer of thickness  $\delta_{opt}$  up to the ablation threshold (see Eq. 3). While the optical absorption depth does not affect the ablation speed,  $AS = \delta_{opt}/t_{abl} = \delta_{opt}/t_{des}$ , it does affect the time required for the tissue to be heated up to ablation. The longer the desiccation time, the more free water gets evaporated and the more likely it is that the water micro-explosive mechanism will be overcome by the mechanism of melting of the dried out tissue. As follows from Eq. 3, the desiccation time is not fully defined by the surface power density, but by the volume power density,  $P_v = P_d / \delta_{opt} = P / (S \delta_{opt})$  (in  $W/mm^3$ ):

$$t_{des} = h_a / P_v \quad . \tag{5}$$

The higher the volume power density, the shorter the desiccation time and consequently also the lower the level of tissue dehydration (see Fig. 12). This has been confirmed also experimentally. For example, the  $CO_2$  laser ablation rate in guinea pig skin was measured to increase by a factor of 1.6 when the volume power density was increased from 64 to 6400 W/mm<sup>3</sup> [19], as expected from the lower level of tissue dehydration at the higher power density. Similarly, charring caused by tissue desiccation was reported to occur more readily at lower  $CO_2$  laser power densities [78, 80].



Fig. 12: Dependence of desiccation time  $t_{det}$  on volume power density  $P_{r}$ .

# **IV. DISCUSSION**

#### a) Effects of tissue desiccation

Our analysis of the Er:YAG and CO<sub>2</sub> laser-tissue interaction demonstrates, in agreement with published experimental data, that the ablative and thermal effects on soft human tissues are very similar for both laser types. This is attributed to the fact that both lasers are predominantly strongly absorbed in the soft tissue's intrinsic water, resulting in the same basic mechanism of interaction with soft tissues. During rapid heating of the confined tissue water, high subsurface pressures are created that lead to the explosive removal of the surrounding tissue material.

Soft-tissue desiccation during laser surgery with mid-IR lasers is an undesirable phenomenon since it reduces the cutting efficacy. Therefore, it is desired that laser parameters and surgical protocols are chosen such that this effect is minimized. However, in general, it does not have a detrimental effect on surgical laser procedures on soft tissues. An exception is procedures on hard tissues that are characterized by low water content, where external water spray needs to be delivered onto the irradiated area in order to re-hydrate the tissue to prevent complete ablation stalling [27-29].

The above considerations apply only for mid-IR wavelengths, where the difference is relatively high between their predominant absorption in water and the underlying absorption in dry substance. In this case, the water micro-explosive mechanism continues to dominate even under partial desiccation conditions (see Fig. 13)



Fig. 13: Depiction of the water mediated micro-explosive ablation mechanism for Er:YAG in partially desiccated soft tissue.

However, when the difference between the absorption in water and dry tissue is relatively small, then even a small level of desiccation can cause the water micro-explosive mechanism to be replaced by the mechanism of melting, carbonization and evaporation of the dry matter (see Fig. 14). This is because in such situations there is no longer an adequate water heat sink to hold the temperature at the water's boiling temperature.



Fig. 14: Depiction of the melting with charring ablation mechanism for  $CO_2$  in partially desiccated soft tissue.

For example, in dental dentin (12% water content) the absorption of Er:YAG (2,940 nm) in the hydrated tissue is approx. 10 times higher than in the desiccated tissue, while for the Er,Cr:YSGG laser (2,730 nm) this ratio is about 3-times smaller [30]. In the absence of water spray, this difference results in carbonized cavities with Er,Cr:YSGG, while clean cavities are achieved with Er:YAG, in spite of the dentin getting desiccated in both cases (Fig. 15) [31].



Fig. 15: Pictures of cavities in dentin, made with Er:YAG and Er,Cr:YSGG lasers following three consecutive laser pulses of the same laser pulse fluence and duration [31].

A similar effect is observed also in soft-tissue surgery with Er:YAG and CO<sub>2</sub> lasers. In this case, the absorption of Er:YAG (2,940 nm) in the hydrated soft tissue is approx. 300 times higher than in the desiccated tissue, while for the CO<sub>2</sub> laser (10,640 nm) this ratio is much smaller, only about 8-times [4]. Therefore, the amount of light absorption in desiccated tissue for the Er:YAG laser is virtually negligible, while for the CO<sub>2</sub> laser interaction, the absorption in the desiccated tissue can he considerable. Assuming that desiccation occurs within the thermal depth, a rough estimate shows that a complete absorption of the CO<sub>2</sub> laser energy by the dry substance will occur within a typical thermal depth of 100 µm. On the other hand, for the Er:YAG laser to be completely absorbed within the desiccated tissue layer, the thermal depth should be much larger, on the order of 900 µm. Consequently, tissue denaturation and charring occurs much more readily during CO<sub>2</sub> soft-tissue surgery.

Soft-tissue ablation is thus governed by the interplay of two opposing effects. On one hand, higher surface power density reduces the desirable thermal depth (See Fig. 8), while on the other hand, higher power density decreases the level of tissue desiccation (See Eq. 5). It is to be noted that for the same surface power density, the volume power density of the Er:YAG laser is about 6 times larger than that of the CO<sub>2</sub> laser, due to the difference in their optical penetration depths. Therefore, for the same surface power density, the tissue gets desiccated faster when irradiated by the CO<sub>2</sub> laser (See Eq. 5). Surgeons using CO<sub>2</sub> laser are therefore advised to avoid using low surface power densities because they cause carbonization [80].

The calculated dependence of the desiccation time on the laser type (optical penetration depth) and surface power density is presented in Table 1.

**Table 1:** Dependence of volume power density  $P_i$ , and consequently of desiccation time ( $t_{des}$ ) on surface power density,  $P_{d}$ . For the same surface power density, the time available for desiccation is higher with the  $CO_2$  laser.

	CO2		Er:YAG	
Surface Power Density (W/cm <sup>2</sup> )	Volume Power Density (W/mm <sup>3</sup> )	Desication time (in ms)	Volume Power Density (W/mm <sup>3</sup> )	Desication time (in ms)
50	29	102.0	167	18.0
100	59	51.0	333	9.0
200	118	25.5	667	4.5
500	294	10.2	1667	1.8
1000	588	5.1	3333	0.9
2000	1176	2.6	6667	0.5
5000	2941	1.0	16667	0.2
10000	5882	0.5	33333	0.1

Experiments show that observable desiccation occurs already for  $CO_2$  laser pulses with  $t_p = 2 \text{ ms}$  [7, 25]. Therefore, in order to avoid excessive desiccation and charring, it is recommended that  $CO_2$  laser surgery is performed at higher surface power densities than with Er:YAG [80], in order to obtain approximately the same or preferably higher volume power density with the  $CO_2$  laser.

A strong hemostatic effect is often reported for the  $CO_2$  laser [42, 43], which can be attributed to tissue desiccation and the associated tissue overheating and charring [78, 80]. While the hemostatic effect of the  $CO_2$  laser as a result of tissue desiccation may be welcome [20], it can also lead to higher post-operative morbidity and complications. It is important to note that excessive thermal injury and damage not only produces erythema, but it can also be associated with angiogenesis, leading to visible telangiectasia, potential hypertrophic scarring and the development of late hypopigmentation [38-41].

As has been shown, the Er:YAG laser the hemostatic and ablative effects can be controllably generated without the risk of charring by appropriately adjusting the laser parameters [35, 44]. When low fluences (below or around the ablation threshold  $\sim 1$ J/cm<sup>2</sup>; see Fig. 3) and low average surface power densities (below approx. 200 W/cm2; see Figs. 5 and 8) are applied to the tissue, strong coagulation effects are observed [35]. Therefore higher fluences (2-5  $J/cm^2$ ) are used for tissue ablation and lower fluences  $(\leq 1 \text{ J/cm}^2)$  for tissue coagulation (see Fig. 3). This can be, for example, simply achieved by changing the laser spot size from small (for ablative high fluences) to large (for coagulative small fluences) by manually adjusting the distance between the treated tissue and the focal point of the surgical handpiece [35]. The ability to use the Er:YAG laser in the ablation or coagulation mode (as needed) without the risk of charring is one of its unique advantages.

# V. CONCLUSIONS

Our study shows that in spite of their large difference in wavelengths, the Er:YAG (2,940 nm) and  $CO_2$  (9,000-11,000 nm) lasers are very similar in terms of their ablation rates and the thermal-diffusion generated peripheral coagulation at the ablation site during soft-tissue surgery. This is because both lasers are predominantly absorbed by the intrinsic tissue water within a very shallow tissue depth of less than 20  $\mu$ m, and therefore their ablative and thermal effects are governed by the same laser-tissue interaction mechanism of micro-explosive "boiling" of the confined tissue water.

The micro-explosive "boiling" of the confined tissue water results in clean cuts without any undesirable excessive thermal damage of the soft tissues [32-35]. Therefore, it is imperative that no significant tissue desiccation occurs during a procedure. Otherwise, tissue overheating with accompanying undesirable carbonization can occur [16, 22, 36, 37, 78, 80]. Here, the Er:YAG is at a significant advantage due to its larger difference between the absorption in the intrinsic water and dry substance. Consequently, undesirable tissue desiccation with resulting tissue charring occurs much more readily when using a CO<sub>2</sub> laser than when operating with an Er:YAG laser [80]. Because of this limitation, many physicians prefer Er:YAG over CO<sub>2</sub> [45-47].

The advantages of Er:YAG soft tissue surgery are: i) Precision in ablation and coagulation; ability to use the Er:YAG laser in ablative or coagulative mode (as needed) without the risk of charring; ii) wider safety window for procedural parameters within which no tissue charring will occur iii) Less postoperative erythema. Because of the lack of thermal injury, postoperative complications are significantly reduced, and the healing is faster; and iii) Minimal risk of scarring.

In conclusion, a major limitation of the  $CO_2$  laser is the thermal injury to the surrounding desiccated tissues, charring and melting of wound margins [76, 77, 80]. This may promote tissue defragmentation and thus frequently makes histopathological evaluation impossible. Therefore, for the majority of minor surgeries the Er:YAG laser is a better choice [76, 77].

## NOTES

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